

1599 Adelaide St. N., Units 301 & 203 London, ON N5X 4E8 P: 519-471-6667

KITCHENER LOCATION

1415 Huron Rd., Unit 225 Kitchener, ON N2R 0L3 P: 519-725-8093

www.sbmltd.ca

sbm@sbmltd.ca

Brock Development Group Inc. 1584 Routledge Park, London, ON N6H 5L6 24 May 2022 SBM-22-1218

Attn: Ms. Michelle Doornbosch

Re: Servicing Feasibility Study

Proposed Residential Development

1170 Fanshawe Park Road East, London, Ontario

1. INTRODUCTION

This Servicing Feasibility Study (Study) has been prepared by Strik, Baldinelli, Moniz Ltd. (SBM) for Brock Development Group Inc. to address the servicing feasibility for the proposed residential development located at 1170 Fanshawe Park Road East, London. The site is approximately 0.37 ha in area.

The site abuts the Stackhouse Avenue Right-Of-Way (ROW) to the west, Fanshawe Park Road E ROW to the south, an existing residential zone in the southeast corner, agricultural lands to the north and neighborhood facility zone to the northeast corner. See the proposed site plan by Brock Development Group enclosed with this Study.

This Study is to determine the adequacy of the existing City services in support of a Zoning Bylaw Application (ZBA), an official Plan Amendment, and the Site Plan Approval (SPA) application for the proposed redevelopment.

Design requirements have been based on the City of London Design Specifications & Requirements Manual (DS&RM), updated March 2022.

2. WATER SERVICING

As per the City's record drawing 27115, dated as constructed February 24, 2017, there is an existing 400mm PVC watermain on south side of Fanshawe Park Road East. The single 25 mm diameter existing water service connection for 1170 Fanshawe Park Road East per City Record drawing 27115 will be proposed to be decommissioned.

2.1 Domestic Water Supply

Domestic water supply will be provided via the existing watermain on Fanshawe Park Road East. The maximum hour domestic demand, as per the DS&RM for the building occupancy load of 63 people (26 Units at 2.4 people per unit) is 1.45 L/s. See the attached domestic water demand calculations.

2.2 Water Supply for Fire Protection

The proposed residential development is a Part 9 building (3-Storeys high or less and less than 600 m²), therefore no sprinkler system is required for this development.

Section 7.3.1 of the DS&RM, updated March 2022, requires the minimal residual pressure in a fire flow scenario to be not less than 140 kPa (20 psi) at any hydrant lateral or fire service connection. Section 7.3.1 of the DS&RM also requires that the maximum residual pressure shall not exceed 550 kPa (80 psi).

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Upon review of the hydrant flow test results (attached to this Study) as tested on November 18, 2015 and using linear interpolation of the residual pressure readings at the provided flow rates from the hydrant, there is sufficient residual pressure within the system. The flow test results show that the static pressure of the water distribution system in the area is 468.84 kPa (68 psi) and the residual pressure is 448.16 kPa (65 psi) at the test flow rate of 4,391 L/min (1160 USGPM). At the required fire flow + maximum day demand rate of 5439 L/min, the residual pressure in the water main would be approximately 457.56 kPa (66.36 psi) which exceeds the minimum required 140 kPa (20 psi) in fire-flow scenarios and does not exceed the maximum residual pressure of 550 kPa (80 psi). Please refer to the calculations attached to this Study.

Based on the current OBC requirements, a fire hydrant should be located 90 m from the subject property's edge of the building. As per the City's record drawing 27115, dated as constructed February 24, 2017, there is an existing municipal hydrant at the southeast side of Fanshawe Park Road East located at a distance which is greater than 90 m from the subject property's edge of the building. Based on the location of the existing hydrant, a new on-site hydrant will be required. The location of the hydrant will be determined at the time of Site Plan Approval.

The fire-fighting flow calculations is determined as per OBC A-3.2.5.7. Since the proposed building is a residential development, the building is classified as group C (Refer to OBC volume 1 table 3.1.2.1). Type of construction is combustible. To be more conservative, water supply coefficient – K is assumed to be 23 (Refer to OBC volume 2 table 1). Building area is equivalent to the most conservative one which is approximately 373.31 m². As per the Site Plan by Brock Development Group attached to this Study, unit 20 abuts units 18 and 22 to the east and west, unit 16 to the north, and the road to the south. Therefore, the spatial coefficient S_{Total} is calculated to be 1.8. Refer to the calculations attached to this Study.

2.3 Water Supply Conclusions

As shown in the attached Domestic and Fire-Flow Water Servicing Calculations (considering the hydrant flow test, OBC A-3.2.5.7 flow demand requirements, and maximum day domestic demand), the water pressure in the Fanshawe Park Road East watermain at the required flow of 5439 L/min (fire flow + maximum day demand), will be around 66.36 psi. It can be concluded that adequate water supply for the proposed development is available from the municipal system with residual pressures greater than the minimum requirement of 140 kPa (20 psi) and does not exceed the maximum requirement of 550 kPa (80 psi).

Based on the above and the Fire-Flow calculations attached, we recommend that a 250 mm diameter water service to be considered for preliminary design purposes for the subject address and proposed development, connected to the existing 400 mm PVC watermain. A new on-site fire hydrant will be required, that will provide the fire protection. Domestic water services will probably be 25 mm per unit, connected to the recommended 250 mm diameter water service.

3. SANITARY SERVICING

The sanitary service connection for the proposed site development is assumed to connect to the existing 150 mm diameter sanitary sewer stub (invert at 252.749) as seen in the City's record drawing 23144 dated March 6, 2012, with the size to be confirmed at the time of Site Plan Approval. As per the City's record drawing 23144 dated March 6, 2012, the site is tributary to the 600 mm diameter sanitary sewer in the Stackhouse Avenue ROW.

The proposed flows from the subject property are shown on the Sanitary Sewer Design Sheet appended to this Study. Using a flow of 230 L/capita/day as per the DS&RM for the building occupancy load of 63 people (26 units at 2.4 people per unit) results in an anticipated peak sanitary flow of 0.79 L/s. When combined with infiltration, this results in a total peak flow of 0.83 L/s. Preliminarily, the existing 150 mm sanitary service stub per City record drawing 23144 at a slope of 7.3% has sufficient capacity to convey these proposed flows and should be considered for preliminary design purposes.

The site is ultimately tributary to the 600 mm diameter sanitary sewer on Fanshawe Park Road East. According to the City's record drawing 23137 Stoney Creek Trunk Sanitary Sewer Design Sheet, dated as constructed January 12, 2012 (Sealed March 6, 2012), the total sewage flow at this location is 223.7 L/s with a capacity of 245.99 L/s (using the sewage flow of 250 L/cap/day). As per 2022 DSRM, the daily flow has been updated in our calculations to reflect 230 L/cap/day. This updated flow combined with the proposed flow of 0.83 L/s produces a total flow of 208.17 L/s which does not exceed the sanitary sewer's capacity of 245.99 L/s. Therefore, there appears to be sufficient capacity in the receiving sewers immediately downstream of the proposed development.

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4. STORM SERVICING AND STORMWATER MANAGEMENT

As per the City's record drawing 27101, dated February 24, 2017, the site is tributary to the existing 675 mm diameter storm sewer on Stackhouse Avenue, with a runoff coefficient (C-value) of 0.72 under existing conditions. The proposed site has an existing 300 mm diameter storm service stub on Stackhouse Avenue (found within EXT'L-1 on the City's record drawing 27101).

A Storm/Drainage Servicing Report demonstrating compliance with the SWM criteria and environmental targets identified in the Stoney Creek Subwatershed Study (quality control of 80% TSS removal) will be assessed at the time of Site Plan Approval.

The SWM calculations attached to this Study show that the post development C-value of 0.74 for the entire site is greater than the allowable C-value of 0.72 per City record drawing 27102. Therefore, storm water management quantity controls are proposed for this development. It is proposed to connect a storm service to the existing storm servicing stub at 2U327 in the Stackhouse Avenue to convey minor flows (2-year allowable storm event), while major flows (up to the 100-year storm event) will be managed (stored) on-site. The 250-year storm event will be safety conveyed overland to the Fanshawe Park Road East ROW or the Stackhouse Avenue ROW. Detailed SWM calculations shall be submitted with the first SPA submission.

5. SUMMARY

Based on the above, the existing city infrastructure and proposed site services have sufficient capacity to accommodate the proposed development of the 0.37 ha subject site located at 1170 Fanshawe Park Road East, London.

6. LIMITATIONS

This Study was prepared by Strik, Baldinelli, Moniz Ltd. for Brock Development Group Inc. and the City of London. Use of this Study by any third party, or any reliance upon its findings, is solely the responsibility of that party. Strik, Baldinelli, Moniz Ltd. accepts no responsibility for damages, if any, suffered by a third party as a result of decisions made or actions undertaken as a result of this Study. Third party use of this Study, without the express written consent of the Consultant, denies any claims, whether in contract, tort, and/or any other cause of action in law, against the Consultant.

All findings and conclusions presented in this Study are based on site conditions as they appeared in the information presented to SBM and related to in this document. This Study is not intended to be exhaustive in scope, or to imply a risk-free development. It should be recognized that the passage of time may alter the opinions, conclusions, and recommendations provided herein, as well as any changes in the layout of the development.

The design was limited to the documents referenced herein and Strik, Baldinelli, Moniz Ltd. accepts no responsibility for the accuracy of the information provided by others. All designs and recommendations presented in this Study are based on the information available at the time of the review.

This document is deemed to be the intellectual property of Strik, Baldinelli, Moniz Ltd. in accordance with Canadian copyright law.

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7. CLOSURE

We trust this Study meets your satisfaction. Should you have any questions or require further information, please do not hesitate to contact us.

Respectfully submitted,

Strik, Baldinelli, Moniz Ltd.

Planning • Civil • Structural • Mechanical • Electrical

Ryan Frouws, P.Eng. Civil Eng II, Project Lead

Encl: Site Plan by Brock Development Group.

City of London record drawings 27115 Domestic Water Demand Calculations

Hydrant Flow Test

Fire Flow Calculations (as per OBC A-3.2.5.7) City of London record drawings 23144 and 23137

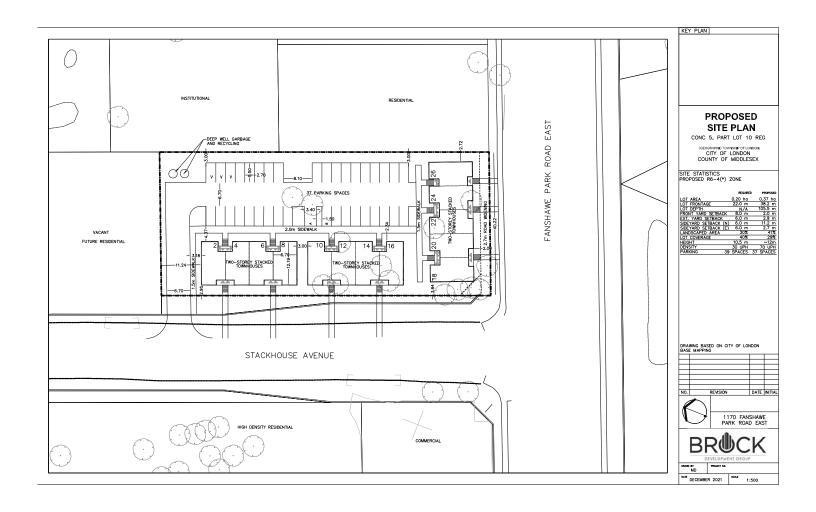
Sanitary Service Design Sheet

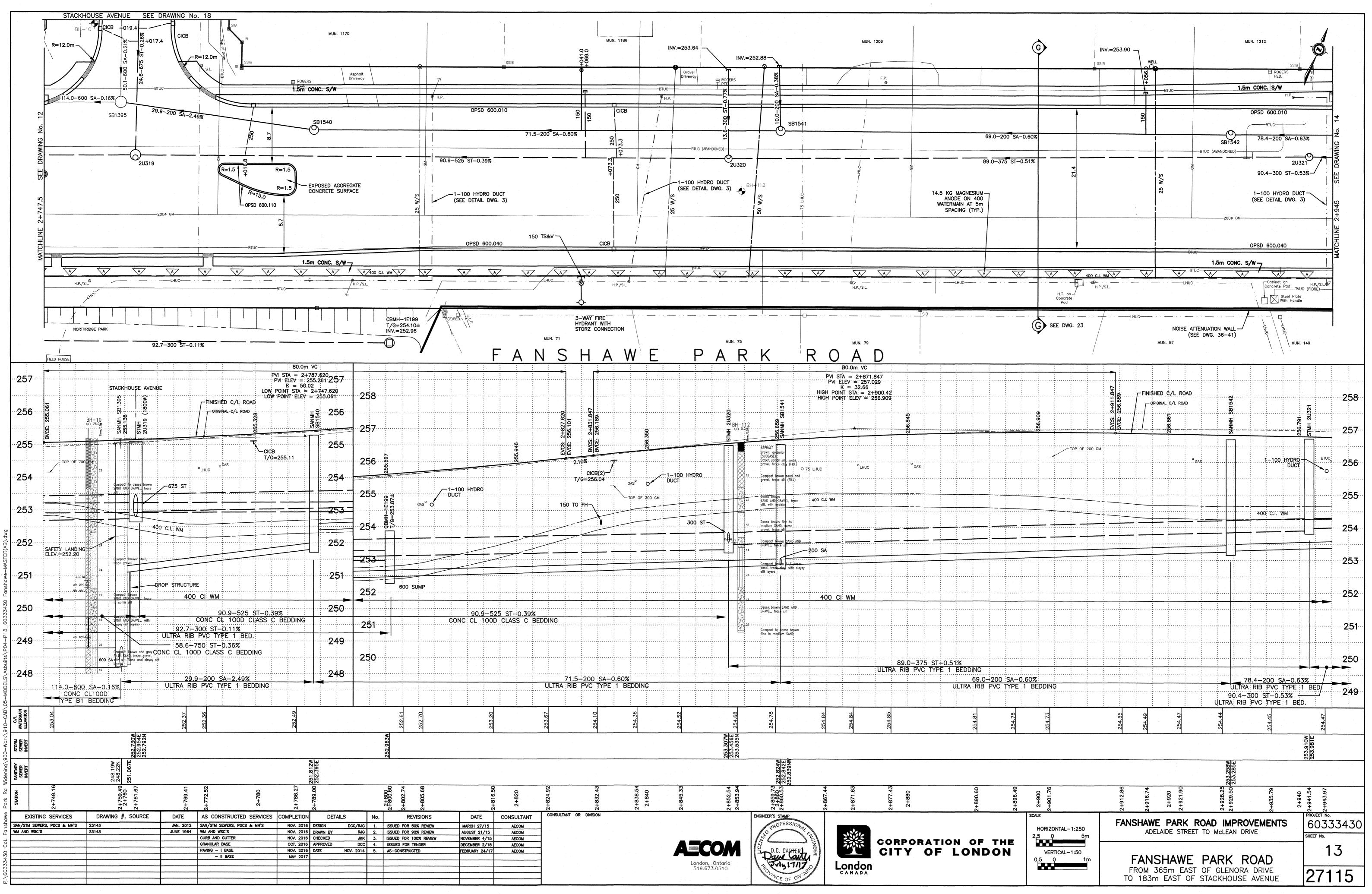
City of London record drawings 27101 and 27102

Runoff Coefficient Calculations



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DOMESTIC WATER DEMAND CALCULATION

DATE: May 24, 2022

JOB NO.: SBM-22-1218

Client: Brock Development Group Inc.
Project: Proposed Residential Development
Location: 1170 Fanshawe Park Road, London, Ontario

**Avg. Day Demand = 255 L/D/cap = 0.002951389 L/s/cap

**Max. Day Peaking Factor = 3.5 **Max. Hour Peaking Factor = 7.8

*Total Building Population = 63 People

	Units	*Population	Avg. Day (L/s)	Max. Hour (L/s)	Max. Day (L/s)
Townhouses	26	63	0.19	1.45	0.65
TOTAL:		63	0.19	1.45	0.65
					39 L/min

VELOCITY CALCULATION

Diameter (mm)	Demand (L/s) - Per Unit	Velocity (m/s)
25	0.06	0.113

Maximum allowable velocity of 1.5 m/s under maximum hour domestic flow conditions as per Section 7.3.6 of the City of London Design Specifications and Requirements Manual.

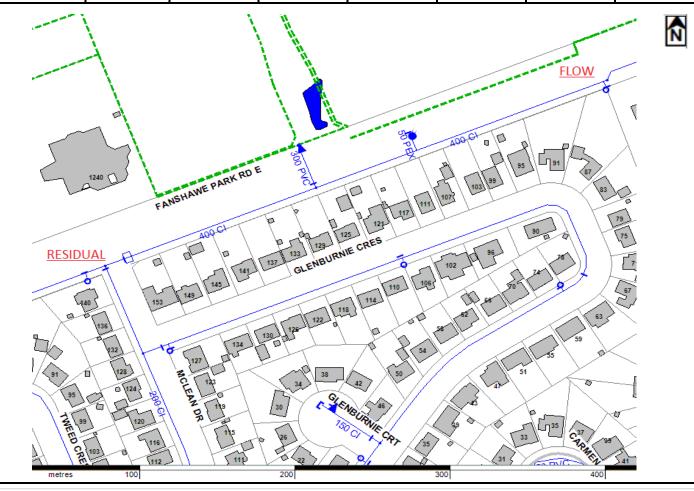
^{*}Residential Building population based on 26 units (Medium density residential) at 2.4 person/unit as per Section 7.3.2.2 in DS&RM.

^{**}Domestic Water Demands from Section 7.3.2.2 in DS&RM

WATER SUPPLY DEPARTMENT FLOW TESTS

DATE:	Wednesday, November 18, 2015		FLOW TEST No.		15-93				
TIME:	9:00 AM		HYDRANT ID						
OPERATOR:	Roger Ham	CHLC	CHLORINE RESIDUAL mg/L						
OPERATOR:	City Operator		GOOD	EXCELLENT					
REQUESTED BY:	Spriet & Assoc - John M. Spriet			>					
LOCATION:	1300 Fanshawe Pk Rd E	TIME USED FOR	5 min						

_			RESIDUAL	HYDRANT			
TEST NUMBER	STATIC PRESSURE P.S.I.	OUTLET SIZE IN.	PITOT READING P.S.I.	INDIVIDUAL FLOW U.S.G.P.M	TOTAL FLOW U.S.G.P.M.	RESIDUAL PRESSURE P.S.I.	STATIC PRESSURE P.S.I.
1	65	2 1/2	48	890	1160	65	68
		2 1/2	30	920			
2					1840	65	
		2 1/2	30	920			



Information contained in this report is representative of flows and pressure losses at the time of the test and depends on reservoir levels, pump operation and customer water demand. Results will vary throughout the day and time of year. Available pressure at other times should be based on a design hydraulic grade line for the pressure zone in which the hydrants are located. By issuing this information report, neither the City nor any of its employees makes any warranty, express or implied, concerning the location, type or extent of services described in this report. Furthermore, neither the City nor any of its employees shall be liable in any manner for any personal injury or property damage or loss of any kind arising from or connected with this information or incomplete information.



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Fire-Fighting Flow (OBC A-3.2.5.7.) Calculations

For data entry
Calculated, not for data entry

DATE: May 20, 2022 JOB NO.: SBM-22-1218

Client: Brock Development Group Inc.
Project: Proposed Stacked Townhouse Development
Location: 1170 Fanshawe Park Rd. E., London, Ontario

Q=K*V*S_{Tot} Fire Flow Demand

Building Classification (3.1.2.1):

Type of Construction:

K (Table 1):

Building Area, m²:

Building Height, m:

Building Volume, m³:

4479.72

 $S_{Tot} = 1.0 + (S_{side1} + S_{side2} + S_{side3} + S_{side4})$ *C

Q, L = 180309

Required Supply Flow Rate, L/min (OBC V2 Table 2) = 5400

**Site Domestic Water Demand, L/min (Max. Day) = Total Required Flow Rate, L/min =

Hydrant Flow Test - 1300 Fanshawe Pk Rd E. Hydrant (H12627) Flow Test - 15-93

psi (468.84 kPa) = L/min (0 USGPM) Static Pressure 68.00 0 Provided Supply Flow Rate @ 68.00 psi (468.84 kPa) = 4391 L/min (1160 USGPM) psi (448.16 kPa) = L/min (1840 USGPM) Provided Supply Flow Rate @ 65.00 6965 psi (457.56 kPa) = L/min (1437 USGPM) Using linear interpolation, residual pressure at hydrant = 66 36 5439

39.00

5439

90LPS

Calculated Pressure Drop = 1 64 Calculated Pressure Drop = 1.15 m head HGL from DS&RM (Low Level System) = 301.80 m Total Head Under Fire Flow Conditions = 300.65 m head Approximate Elevation of Proposed Connection = 252.51 m*** Total Pressure Head = 48.14 m head

Water Pressure Under Firefighting Conditions Excluding Losses = 48.14 m head (68.45 psi, 471.97 kPa)

Therefore, water supply pressure at the proposed building under fire flow conditions not accounting for losses = 48.14 m head (68.45 psi, 471.97 kPa) which is greater than 140 kPa (20 psi) required per Section 7.3.1 of the City of London DS&RM.

- *Refer to attached Figure 1 (Spatial Coefficient vs Exposure Distance)
- **Refer to attached Domestic Water Demand Calculations.
- ***Assumed From Plan and profile as built drawing 27115. To be confirmed at a later stage.

q = volume flow (L/s) [refer to fire-fighting demand calculations]

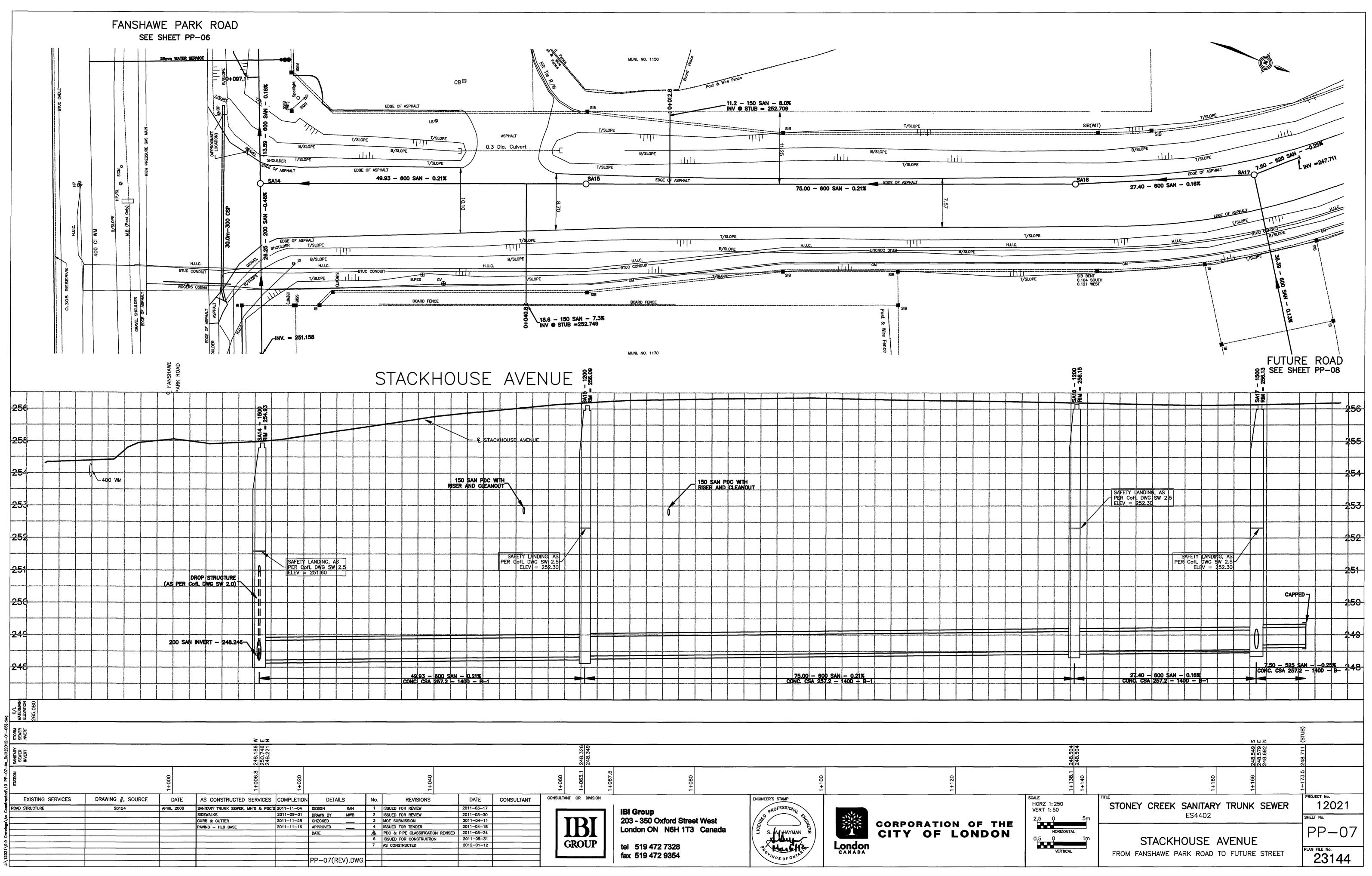
d = inside or hydraulic diameter (mm) [refer to drawing C3]

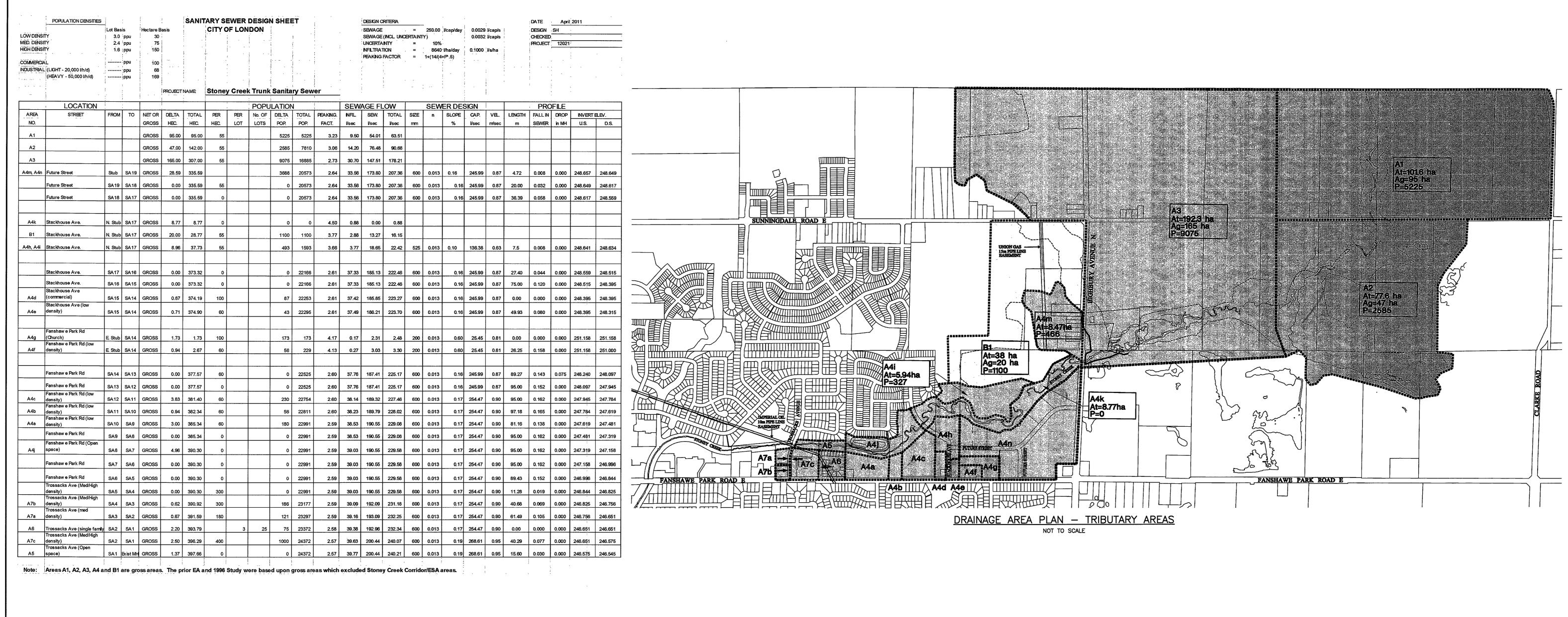
90.7	L/s
250	mm

Calculated Flow Velocity

v = flow velocity (m/s)

1.85





LEGEND

DRAINAGE AREA BOUNDARY

APPROXIMATE ESA/PSW/CREEK BOUNDARY

(TAKEN OUT OF At)

A2 AREA ID.

At=40 ha TOTAL AREA IN HECTARES

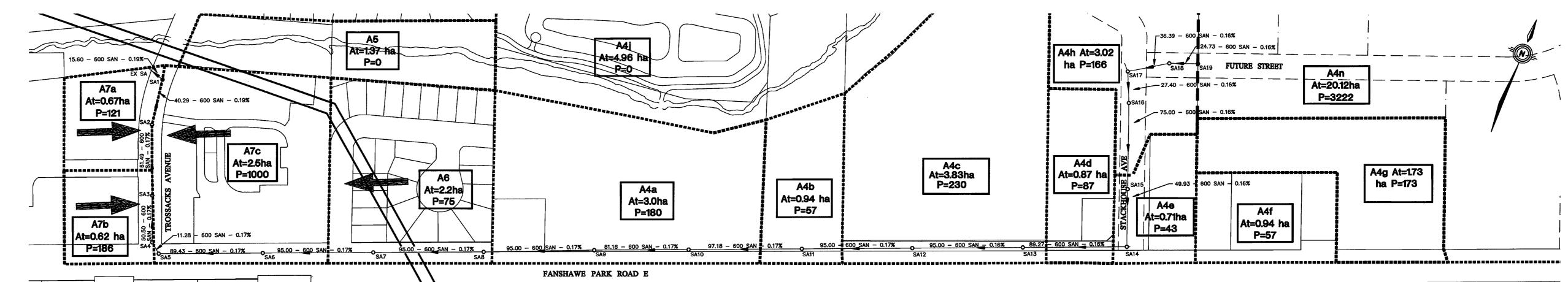
GROSS AREA IN HECTARES

(TOTAL AREA MINUS AN ESTIMATED AREA FOR THE STONEY CREEK CORRIDOR)

POPULATION

SYPHON UNDER STONEY CREEK.

NOTES:
AREAS A1, A2, A3 AND A4 AS PER "CITY OF LONDON SANITARY SEWAGE SERVICING STUDY 20 YEAR PLAN" STANLEY ASSOCIATES, MAY 1996.
AREAS A3 AND A4 ADJUSTED BASED ON KILALLY NORTH SANITARY TRUNK SEWER STUDY (CLASS EA 2001), AND DRAINAGE AREAS ON MARSMAN LANDS RECEIVED FROM THE CITY OF LONDON ON MARCH 30, 2011.
POTENTIAL OVERLAP AREA FROM FUTURE SUBDIVISION (AREA B1), INCLUDED AT CITY'S REQUEST.
AREAS A6 AND A7 DIVERTED FROM EXISTING SANITARY



CONS	CONSULTANT	DATE	REVISIONS	No.	AILS	DETA	COMPLETION	AS CONSTRUCTED SERVICES	DATE	DRAWING #, SOURCE	EXISTING SERVICES
		2011-03-17	ISSUED FOR REVIEW	1	SAH	DESIGN					
		2011-03-30	ISSUED FOR REVIEW	2	SAH/JCW	DRAWN BY					
		2011-04-11	MOE SUBMISSION	3	RCW	CHECKED					
		2011-04-18	ISSUED FOR TENDER	4	SAH	APPROVED					
		2012-01-12	AS CONSTRUCTED	5	2011-03-07	DATE			'		
					DWC	SA-01.					
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BI GROUP

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203 - 350 Oxford Street West
London ON N6H 1T3 Canada

tel 519 472 7328 fax 519 472 9354





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10	Q	20m	
	HORIZON	ITAL	

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STONEY	CREEK	SANITARY	TRUNK	SEWER
		ES4402		
				

SANITARY DRAINAGE AREAS

PLAN FILE NO. 23137

SA-0

12021



Sanitary Service Design Sheet City of London

Residential Population Densities

(A) Area Basis

Low Density Residential (Single Family/Semi-Deta = 30 Units/hectare @ 3 people/unit

Medium Density Residential (Multi-Family/Tow =75 Units/hectare @ 2.4 people/unit

High Density Residential (Apartment Buildings) =150-300 Units/hectare @ 1.6 people/unit

Commercial = 100 people/hectare

Daily Flow (L/cap/day) 250
Daily Flow (L/cap/day) 230
Sewage Infiltration (Litres/hectare/day) 8640
Harmon Formula (Peaking Factor)

 $M = (1 + 14/(4+P^0.5))$ Uncertainty Factor 1.1 **Date:** May 11, 2022 **Job Number:** SBM-22-1218

Client: Brock Development

Project: Proposed Residential Development **Location:** 1170 Fanshawe Park Road E.

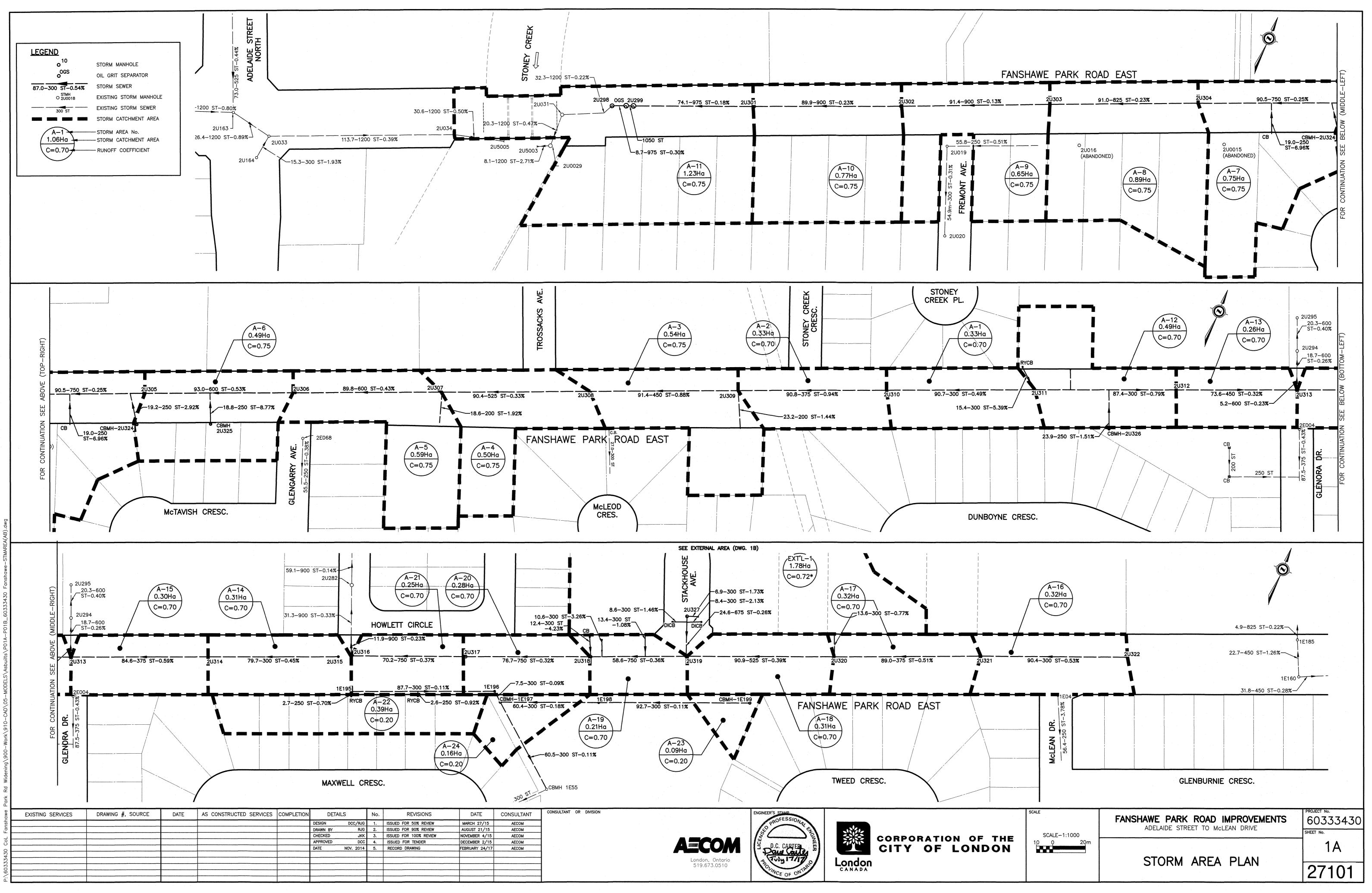
Designed By: RS Reviewed By: RF

Location Area Population									Sewage Flows Sewer design												
LO	Jeanon	1	AI	Ca			Population	1	T	Jewage Flows					Jewei design						
Area No.	From MH	To MH	Delta Hectare	Total Hectare	*No. of Units	**People Per Unit	People Per Hectare	Delta Pop.	Total Pop.	Harmon Peaking Factor	Infilt L/S	1 -		Pipe n Slope %		Dia. mm	Capacity L/S	Velocity m/s			
***Upstream Conditions																					
Area 4d	SA15	SA14	0.87	374.19	0	0.0	100	87	22253	2.61	37.42	184.58	222.00	0.013	0.16%	600	245.75	0.87			
***Existing Condition (A4e)																				
Area 4e	SA15	SA14	0.71	374.9	0	0.0	60	42.6	22296	2.61	37.49	170.09	207.58	0.013	0.16%	600	245.75	0.87			
Proposed Condition																					
Medium Density	SA15	SA14	0.37	0.37	26	2.4		62.4	63	4.29	0.04	0.79	0.83	0.013	7.30%	150	41.17	2.33			
***Downstream Condition	S																				
Area 4e	SA15	SA14	0.71	375.61	26	2.4	60	62.4	22379	2.60	37.56	170.61	208.17	0.013	0.16%	600	245.75	0.87			

^{*}Based on Proposed site plan by Brock Development Group

^{**}Medium Density Residential (Multi-family/Townhouse) 75 Units/hectare @ 2.4 people/unit

^{***}Based on City of London Record Drawing 23144



RUNOFF COEFFICIENT 'C'

PARKS & PLAYGROUNDS

- 0.20

RESIDENTIAL- SINGLE & DUPLEX - 0.40 to 0.50

- APARTMENTS COMMERCIAL & INDUSTRIAL

- ROWHOUSING

- 0.65 - 0.65 to 0.70

- 0.90 & 0.70 - 0.90 DENSELY BUILT, PAVED

FLOW, Q = 2.78 CIA

WHERE Q = PEAK FLOW IN LITRES PER SECOND (L/s)

C = RUNOFF COEFFICIENT (See Above) i = RAINFALL INTENSITY (mm/hr), RETURN PERIOD = 2 years

A = AREA IN HECTARES (ha)

STORM SEWER DESIGN SHEET

(BASED ON CITY OF LONDON 2-YR STORM)

PROJECT Fanshawe Park Road Widening

PROJECT NO. 60333430

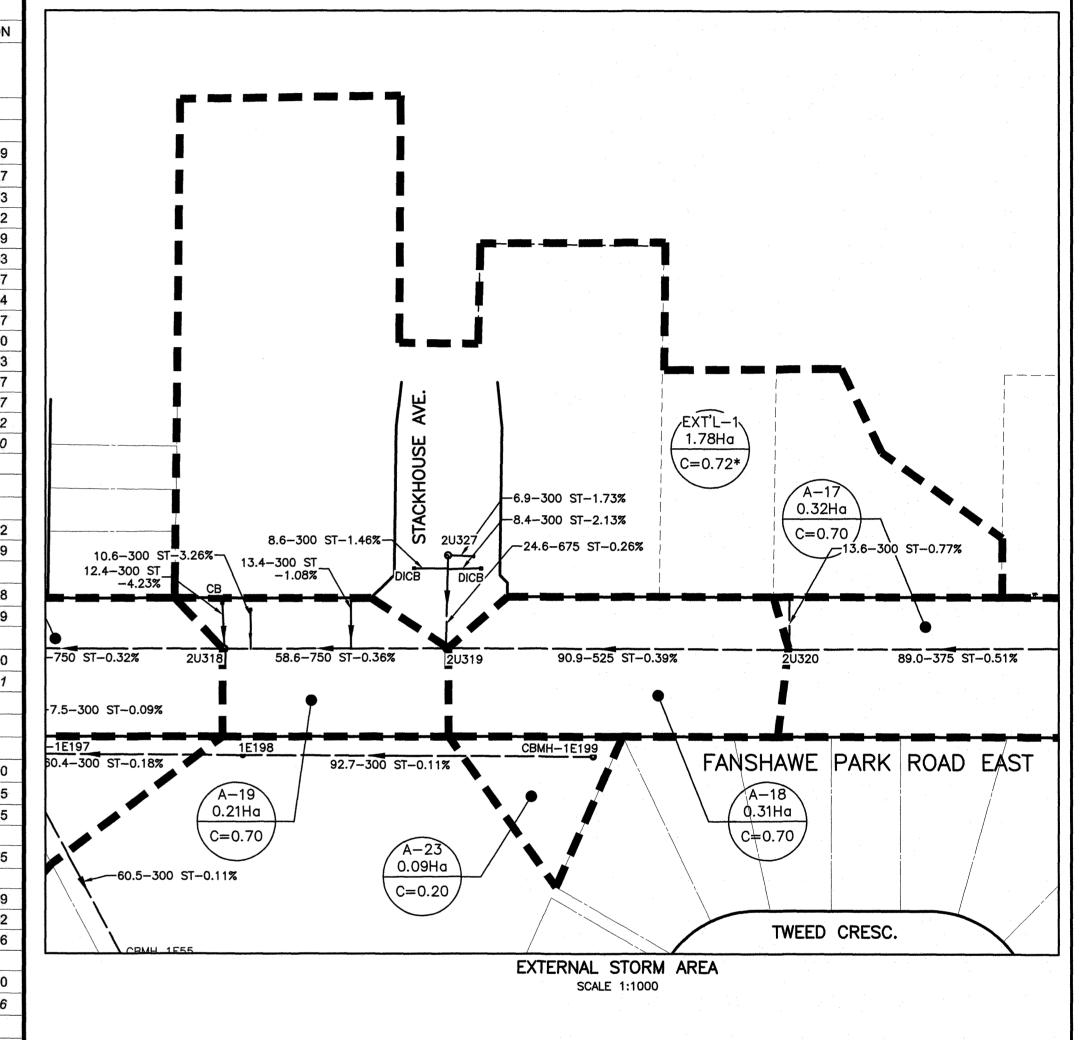
DRAINAGE AREA

DESIGNED BY RJG CHECKED BY DCC DATE 12/01/15

FANSHAWE PARK ROAD WIDENING

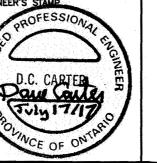
FANSHAWE	PARK ROAD	WIDENING

A1 FAN A2 FAN A3 FAN A4 FAN	STREET JTLET #1 - STONEY CREEK	FROM MH	TO MH				TOT.	RUNOFF	INCR	TOTAL	TOTAL	CUM. SEWER	TIM	ENT	NET LIGHT		"n"	NOM.	STORM	CAPACITY	VELOCITY	TENCOTE	EL OW	SEWER	DROP IN	IN VEDT	
A1 FAN A2 FAN A3 FAN A4 FAN	JTLET #1 - STONEY CREEK	МН	МН							OCIVII OLYTLIN	: 1 11411	E ENT.	INTENSITY		. 11	INCIVI.	OFCIVIV	CAPACITI	VELUCITY	LENGTH	FLOW	SEVVER	DROP IN	INVERT	ELEVATION		
A1 FAN A2 FAN A3 FAN A4 FAN	JTLET #1 - STONEY CREEK		1500 1	AREA	AREA	COEFF.	AxC	SECT. AxC	LAT.	(2.78 x)	SECT.	ACCUM.	'i'			PIPE D	SLOPE	Q	m./s.	-	TIME	FALL	MANHOLE	U.S.	D.S.		
A1 FAN A2 FAN A3 FAN A4 FAN	JTLET #1 - STONEY CREEK			ha.	ha.	(above)		AXC	AXC	AxC	min.	min.	mm/hr	l/s		mm	%	I/s	(min. 1.0 m/s	m	minutes	m	m	m	m		
A1 FAN A2 FAN A3 FAN A4 FAN	P. B. Bargine, B. B. St. T. Sept. B. Sept. St. St. Sept. St. St. Sept. St. Sept. St. St. Sept. S			3.77				,,,,,,		7	1							:	(0.000		THE TAXABLE PARTY		1	***			
A2 FAN A3 FAN A4 FAN	retakanan erretakan erretakan angan manangan erretakan dari penara a mengenara a sa mengenara dari penara angan					-											.,	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·		<u> </u>					
A2 FAN A3 FAN A4 FAN	NSHAWE PARK ROAD E.	1	2	0.33	0.33	0.70	0.23			0.64		12.50	95.16	61.11	0.013	300	0.54	74.14	1.05	91.0	1.45	0.49		252.720	252.229		
A3 FAN A4 FAN	NSHAWE PARK ROAD E.	2	3	0.33	0.66	0.70	0.23	0.23		1.28	1.45	13.95	90.15	115.78	0.013	375	0.70	153.05	1.39	91.0	1.09	0.43	0.075	252.154	251.517		
A4 FAN	NSHAWE PARK ROAD E.	3	4	0.54	1.20	0.75	0.41	0.46		2.41	1.09	15.04	86.68	208.92	0.013	450	0.90	282.21	1.77	91.0	0.85	0.82	0.075	251.442	250.623		
A5 FAN	NSHAWE PARK ROAD E.	4	5	0.50	1.70	0.75	0.38	0.87		3.45	0.85	15.90	84.14	290.52	0.013	525	0.45	301.01	1.39	91.0	1.09	0.41	0.211	250.412	250.023		
	NSHAWE PARK ROAD E.	5	6	0.59	2.29	0.75	0.44	1.24		4.68	1.09	16.99	81.10	379.79	0.013	600	0.45	429.28	1.52	91.0	1.00	0.41	0.075	249.927	249.519		
A6 FAN	NSHAWE PARK ROAD E.	6	. 7	0.49	2.78	0.75	0.37	1.68	***************************************	5.70	1.00	17.98	78.49	447.78	0.013	600	0.55	475.11	1.68	91.0	0.90	0.50	0.025	249.494	248.993		
A7 FAN	NSHAWE PARK ROAD E.	7	8	0.75	3.53	0.75	0.56	2.05		7.27	0.90	18.89	76.27	554.37	0.013	750	0.25	580.78	1.31	91.0	1.15	0.23	0.699	248.294	248.067		
A8 FAN	NSHAWE PARK ROAD E.	8	9	0.89	4.42	0.75	0.67	2.61		9.12	1.15	20.04	73.60	671.53	0.013	825	0.25	748.85	1,40	91.0	1.08	0.23	0.075	247.992	247.764		
22 23 27 27	NSHAWE PARK ROAD E.	9	10	0.65	5.07	0.75	0.49	3.28		10.48	1.08	21.12	71.25	746.64	0.013	900	0.20	844.71	1.33	91.0	1.14	0.18	0.075	247.689	247.507		
	NSHAWE PARK ROAD E.	10	11	0.77	5.84	0.75	0.58	3.77		12.08	1.14	22.27	68.92	832.87	0.013	900	0.20	844.71	1.33	91.0	1.14	0.18	0.025	247.482	247.300		
	NSHAWE PARK ROAD E.	11	OGS	1.23	7.07	0.75	0.92	4.35		14.65	1.14	23.41	66.73	977.55	0.013	975	0.20	1045.70	1.40	91.0	1.08	0.18	0.075	247.225	247.043		
	NSHAWE PARK ROAD E.	OGS	12	0.00	7.07	0.75	0.00	5.27	, , , , , , , , , , , , , , , , , , , ,	14.65	1.08	24.49	64.77	948.88	0.013	975	0.20	1045.70	1.40	5.5	0.07	0.01	0.075	246.968	246.957		
	NSHAWE PARK ROAD E.	12 EX. 2U0031	EX. 2U0031	0.00	7.07	0.75	0.00	5.27		14.65	0.07	24.56	64.66	947.20	0.013	1200	0.28	2156.33	1.91	22.4	0.20	0.06	0.047	246.910	246.847		
	NSHAWE PARK ROAD E. NSHAWE PARK ROAD E.	EX. 200031	EX. 2U0029 OUTLET	0.00	7.07 7.07	0.75	0.00	5.27 5.27		14.65	0.20	24.75	64.32	942.21	0.013	1200	0.47	2779.85	2.46	20.3	0.14	0.09	0.270	246.577	246.482		
- FA	INGITAWE FARR ROAD E.	LA. 200029	COILEI	0.00	7.07	0.75	0.00	0.21		14.65	0.14	24.89	64.08	938.72	0.013	1200	2.71	6696.49	5.92	9.4	0.03	0.25	0.268	246.214	245.960		
OU	JTLET #2 - 1010-1066 FANSHAWE PARK RD.	CONDO SITE											* .		-			1 :	<u> </u>			_					
177,14		<u> </u>				Annual principles and the second seco					,											· · · · · · · · · · · · · · · · · · ·					
A12 FAN	NSHAWE PARK ROAD E.	1	13	0.49	0.49	0.70	0.34			0.95		12.50	95.16	90.74	0.013	300	0.85	93.02	1.32	86.7	1.10	0.74		252.019	251.282		
	NSHAWE PARK ROAD E.	13	14	0.26	0.75	0.70	0.18	0.34		1.46	1.10	13.60	91.31	133.26	0.013	450	0.30	162.93	1.02	74.3	1.21	0.22	0.150	251.132	250.909		
30.34.7.4	Control and Control of State and State and Control			, 4,000,00	7 1 N 7		77.7-	: = (=		21.54	1,,,,,	10.00	<u> </u>	1.46.10.10.	0.0.0	,	,0,00		1,122		5.000.7	1	0.100	201.102	200.000		
A14 FAI	NSHAWE PARK ROAD E.	15	16	0.31	0.31	0.70	0.22		Manager and the second	0.60		12.50	95.16	57.41	0.013	300	0.54	74.14	1.05	80.0	1.27	0.43		252.040	251.608		
	NSHAWE PARK ROAD E.	16	14	0.30	0.61	0.70	0.21	0.22		1.19	1.27	13.77	90.73	107.70	0.013	375	0.60	141.70	1.28	84.0	1.09	0.50	0.075	251.533	251.029		
· · · · · · · · · · · · · · · · · · ·									, , , , , , , , , , , , , , , , , , , ,												1,,,,,,,	1	0,0,0	201.000	2011020		
101	10/1066 FANSHAWE PARK RD. CONDO SITE	14	EX. PLUG	0.00	1.36	0.70	0.00		0.95	2.65		13.68	91.05	240.96	0.013	600	0.25	320.32	1.13	4.2	0.06	0.01	0.158	250.751	250.740		
101	10/1066 FANSHAWE PARK RD. CONDO SITE	EX. PLUG	EX. STMH	0.00	1.36	0.70	0.00	0.95		2.65	0.06	13.74	90.84	240.59	0.013	600	0.25	320.32	1.13	19.7	0.29	0.05	0.000	250.740	250.691		
														#NA 51/4-15			***************************************			37,77	15 7.200						
OU	JTLET #3 - HOWLETT CIRCLE				en e																	1					
													***************************************		· · · · · · · · · · · · · · · · · · ·			· · · · · · · · · · · · · · · · · · ·				 		 			
A16 FAI	NSHAWE PARK ROAD E.	17	18	0.32	0.32	0.70	0.22			0.62		12.50	95.16	59.26	0.013	300	0.54	74.14	1.05	90.0	1.43	0.49		254.476	253.990		
A17 FAN	NSHAWE PARK ROAD E.	18	19	0.32	0.64	0.70	0.22	0.22		1.25	1.43	13.93	90.20	112.34	0.013	375	0.50	129.35	1.17	90.0	1.28	0.45	0.075	253.915	253.465		
A18 FAI	NSHAWE PARK ROAD E.	19	20	0.31	0.95	0.70	0.22	0.45		1.85	1.28	15.21	86.16	159.29	0.013	525	0.40	283.79	1.31	90.0	1.14	0.36	0.150	253.315	252.955		
					AMARIAN TERMANAN ANNA ANNA ANNA ANNA ANNA ANNA ANN													24 - 14 - 14 - 14 - 14		47 - 24-24		200 400					
XT'L-1 ST/	ACKHOUSE AVENUE	20A	20	1.78	1.78	0.72	1.28			3.56		12.30	95.89	341.65	0.013	675	0.25	438.52	1.23	24.0	0.33	0.06		252.865	252.805		
														,													
A19 FAN	NSHAWE PARK ROAD E.	20	.21	0.21	1.16	0.70	0.15		1.95	5.82	1.14	13.23	92.58	538.84	0.013	750	0.35	688.17	1.56	59.7	0.64	0.21	0.225	252.730	252.519		
A20 FAN	NSHAWE PARK ROAD E.	21	22	0.28	1.44	0.70	0.20	2.09	,	6.37	0.64	13.86	90.42	575.52	0.013	750	0.35	688.17	1.56	77.7	0.83	0.27	0.025	252.494	252.222		
A21 FAN	NSHAWE PARK ROAD E.	22	23	0.25	1.69	0.70	0.18	2.29		6.85	0.83	14.70	87.74	601.19	0.013	750	0.35	688.17	1.56	68.7	0.74	0.24	0.025	252.197	251.956		
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	DWLETT CIRCLE	23	EX. 900 ST	0.00	1.69	0.70	0.00	2.46		6.85	0.74	15.43	85.50	585.83	0.013	900	0.13	681.03	1.07	9.9	0.15	0.01	0.163	251.793	251.780		
HO	DWLETT CIRCLE	EX. 900 ST	EX. STMH	0.00	1.69	0.70	0.00	2.46		6.85	0.15	15.58	85.05	582.71	0.013	900	0.13	681.03	1.07	33.9	0.53	0.04	0.000	251.780	251.736		
-										*																	
OU.	JTLET #4 - MAXWELL CRESCENT																		<u> </u>		-		ļ				
		—			<u> </u>									3.35 S-7		12/2/-	2 20 3	g_ 320	42	25.5	2 200 1	<u> </u>					
	NSHAWE PARK ROAD E.	24	25	0.39	0.39	0.20	0.08	200		0.22	3 00	19.00	76.00	16.48	0.013	300	0.30	55.26	0.78	87.9	1.87	0.26	11122	252.513	252.249		
FAD	NSHAWE PARK ROAD E.	25	CBMH-26	0.00	0.39	0.20	0.00	0.08		0.22	1.87	20.87	71.78	15.56	0.013	300	0.30	55.26	0.78	7.9	0.17	0.02	0.050	252.199	252.175		
ADD FIG	DTUDINGE BADIA	CBMU 07	00	0.00	0.00	1	0.00			A 65	<u> </u>	10.00	70.00	0.00	0.040	000	0.00	ep aa	A 70		1			APA			
	DRTHRIDGE PARK	CBMH-27 28	28 CBMH-26	0.09	0.09	0.20	0.02	0.00	_	0.05	4.00	19.00	76.00	3.80	0.013	300	0.30	55.26 55.26	0.78	93.0	1.98	0.28	0.000	252.684	252.405		
INUI	DRTHRIDGE PARK	40	CBMH-26	0.00	0.09	0.20	0.00	0.02		0.05	1.98	20.98	71.55	3.58	0.013	300	0.30	55.26	0.78	60.0	1.28	0.18	0.025	252.380	252.200		
A24 NO	DRTHRIDGE PARK	CBMH-26	EX. CBMH	0.16	0.64	0.20	0.03		0.10	0.36		20.89	71.74	25.53	0.043	300	0.30	55.26	0.78	60.0	1.28	0.46	0.050	252.450	054 070		
	ALWAY TO MAXWELL CRESC.	EX. CBMH	EX. STMH	0.16	0.64	0.20	0.03	0.13	0.10	0.36	1 20	20.89	69.10		0.013 0.013	300	0.30	76.84	1.09	60.0 37.2	0.57	0.18 0.22	0.050 0.050	252.150 251.920			
	marry no. 1 C 1200 (CAST Indiana SCI Min CO)	noness Selectives I	ZA. OTIVIT	3.00	V1975	1	J.00	0.10		V.50	1.40	24.11	03.10	27,03	0.013	300	0.00	70.07	1.03	31.2	0.07	0.22	0.000	201.920	201./04		
						1					1				<u> </u>							_					



EXISTING SERVICES	DRAWING #, SOURCE	DATE	AS CONSTRUCTED SERVICES	COMPLETION	DETAILS	No.	REVISIONS	DATE	CONSULTANT	CC
					DESIGN DCC/RJG	1.	ISSUED FOR 50% REVIEW	MARCH 27/15	AECOM	
					DRAWN BY RJG	2.	ISSUED FOR 90% REVIEW	AUGUST 21/15	AECOM	
					CHECKED JKK	3.	ISSUED FOR 100% REVIEW	NOVEMBER 4/15	AECOM	
	·				APPROVED DCC	4.	ISSUED FOR TENDER	DECEMBER 2/15	AECOM	
					DATE NOV. 2014	5.	RECORD DRAWING	FEBRUARY 24/17	AECOM	
	-									
					·			-		
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FANSHAWE PARK ROAD IMPROVEMENTS
ADELAIDE STREET TO MCLEAN DRIVE

STORM DESIGN SHEET

27102

PROJECT No. 60333430

1B



1599 Adelaide St. N., Units 301 & 203 London, ON N5X 4E8 P: 519-471-6667

KITCHENER LOCATION

1415 Huron Rd., Unit 225 Kitchener, ON N2R 0L3 P: 519-725-8093

www.sbmltd.ca

sbm@sbmltd.ca

Runoff Coefficient Calculations

DATE: May 3, 2022

JOB No.: SBM-22-1218

Client: Brock Development Group Inc.
Project: Proposed Residential Development

Location: 1170 Fanshawe Park Road, London, Ontario

PRE-DEVELOPMENT AREA (TOTAL SITE)

	*Area (m²)	С	AxC
Total Area:	3722.04		
Building Area:	426.10	0.9	383.49
Concrete/Asphalt:	168.00	0.9	151.2
Gravel:	0.00	0.7	0
Landscaped/Open:	3127.94	0.2	625.588
Totals:	3722.04		1160.278
$C_{eq} = \sum (A*C)/\sum (A) =$	0.40	_	
Callowable	0.72	City record drawing 27102	

POST-DEVELOPMENT AREA (TOTAL SITE)

	*Area (m²)	С	AxC
Total Area:	3722.04		
Building Area:	954.82	0.9	859.338
Green Roof:	0.00	0.6 *	0
Concrete/Asphalt:	1599.53	0.9	1439.577
Gravel:	0.00	0.7	0
Landscaped/Open	1167.69	0.4 *	467.076
Totals:	3722.04	_	2765.991
$C_{eq} = \sum (A*C)/\sum (A) =$	0.74		

^{*} Pre-Development Areas are approximate and taken from CAD drawings - City of London Mapping - Topo 2015 - 2D - 7964t_15